BLACKSTONE RIVER BASIN WORCESTER, MASSACHUSETTS

> LEESVILLE POND DAM MA 00141

# PHASE I INSPECTION REPORT NATIONAL DAM INSPECTION PROGRAM

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DEPARTMENT OF THE ARMY
NEW ENGLAND DIVISION, CORPS OF ENGINEERS
WALTHAM, MASS. 02154

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# LEESVILLE POND DAM MA 00141

BLACKSTONE RIVER BASIN WORCESTER, MASSACHUSETTS

PHASE I INSPECTION REPORT NATIONAL DAM INSPECTION PROGRAM

# NATIONAL DAM INSPECTION PROGRAM

#### PHASE I INSPECTION REPORT

#### BRIEF ASSESSMENT

Identification No.: MA00141

Name of Dam: Leesville Pond

Town: Worcester

County and State: Worcester County, Massachusetts

Stream: Kettle Brook - Tributary of Blackstone River

Date of Inspection: July 24, 1978

Leesville Pond Dam is an earthfill dam with a stone masonry spillway section. The dam was originally constructed in about 1830 and has undergone reconstruction and numerous modifications. The dam is about 220 feet long, 15 feet high with an 83.6-foot-long spillway. The earth embankment has a wood plank core wall. The outlet controls consists of two inoperable wooden slide gates. There are no flashboards on the spillway.

Due to its age, Leesville Pond Dam was neither designed nor constructed by current approved, state-ofthe-art procedures. Based upon the visual inspection at the site and a review of the engineering data available, there are areas of concern which must be corrected to assure the continued performance of this dam. erally, the dam is considered to be in fair condition. However, there are several visible signs of distress which may indicate a potential hazard at this site. These are as follows: seepage at the north spillway abutment, slumping and erosion on the upstream face of the dam, inoperable slide gates, leakage around the slide gates, erosion of the earthfill abutment slopes, minor spalling and cracking of the concrete in the discharge channel walls, trees and brush on the dam, and accumulation of debris in the spillway channel.

There is limited residential property immediately downstream of Leesville Pond Dam. For this reason, the dam has been classified in the "significant" hazard category, however, a failure of the dam could affect Curtis Pond Dam and in turn jeopardize the Webster Square area of Worcester.

Hydraulic analyses indicate that the existing spillway without flashboards can discharge a flow of 1,594 cubic feet per second (cfs) at Elevation (E1) 488.3 which is the low area along the top of the dam. An outflow test flood of 8,600 cfs would overtop the north abutment of the spillway, which is the lowest point on the main dam, by about 5.3 feet. The remainder of the dam would be overtopped by about 3 feet. The spillway can discharge only 19 percent of the test flood and is therefore inadequate.

In the event the dam fails, a hazard does exist for the downstream inhabitants due to the effect upon Curtis Pond. Because of this potential hazard and the lack of available design and construction data, it is recommended that the Owner employ a qualified consultant to investigate the seepage and stability of the dam. In addition, the Owner should repair the slumping of the upstream face and replace the riprap. Also, it is recommended that the Owner remove the brush and trees on the dam, clear all debris from the spillway, and repair the outlet structure.

The recommendations and remedial measures described in Section 7 should be implemented by the Owner within a period of 1 year after receipt of this Phase I Inspection Report. An alternative to these recommendations would be draining the reservoir and breaching or removing the dam.

Edward M. Greco, P.E. Project Manager Metcalf & Eddy, Inc.

Connecticut Registration No. 08365

BISHOP

Approved by:

Stephen L. Bishop, P.E.

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Vice President
Metcalf & Eddy, Inc.

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This Phase I Inspection Report on Leesville Pond Dam has been reviewed by the undersigned Review Board members. In our opinion, the reported findings, conclusions, and recommendations are consistent with the Recommended Guidelines for Safety Inspection of Dams, and with good engineering judgment and practice, and is hereby submitted for approval.

CHARLES G. TIERSCH, Chairman Chief, Foundation and Materials Branch Engineering Division

FRED J. RAVENS, Jr., Member Chief, Design Branch Engineering Division

SAUL C. COOPER, Member Chief, Water Control Branch Engineering Division

APPROVAL RECOMMENDED:

JOE B. FRYAR Chief, Engineering Division This report is prepared under guidance contained in Recommended Guidelines for Safety Inspection of Dams, for a Phase I Investigation. Copies of these guidelines may be obtained from the Office of Chief of Engineers, Washington, D. C. 20314. The purpose of a Phase I Investigation is to identify expeditiously those dams which may pose hazards to human life or property. The assessment of the general condition of the dam is based upon available data and visual inspections. Detail investigation, and analyses involving topographic mapping, subsurface investigations, testing, and detailed computational evaluations are beyond the scope of a Phase I investigation; however, the investigation is intended to identify any need for such studies.

In reviewing this report, it should be realized that the reported condition of the dam is based on observations of field conditions at the time of inspection along with data available to the inspection team. In cases where the reservoir was lowered or drained prior to inspection, such action, while improving the stability and safety of the dam, removes the normal load on the structure and may obscure certain conditions which might otherwise be detectable if inspected under the normal operating environment of the structure.

It is important to note that the condition of a dam depends on numerous and constantly changing internal and external conditions, and is evolutionary in nature. It would be incorrect to assume that the present condition of the dam will continue to represent the condition of the dam at some point in the future. Only through continued care and inspection can there be any chance that unsafe conditions be detected.

Phase I inspections are not intended to provide detailed hydrologic and hydraulic analyses. In accordance with the established Guidelines, the Spillway Test flood is based on the estimated "Probable Maximum Flood" for the region (greatest reasonably possible storm runoff), or fractions thereof. Because of the magnitude and rarity of such a storm event, a finding that a spillway will not pass the test flood should not be interpreted as necessarily posing a highly inadequate condition. The test flood provides a measure of relative spillway capacity and serves as an aid in determining the need for more detailed hydrologic and hydraulic studies, considering the size of the dam, its general condition and the downstream damage potential.

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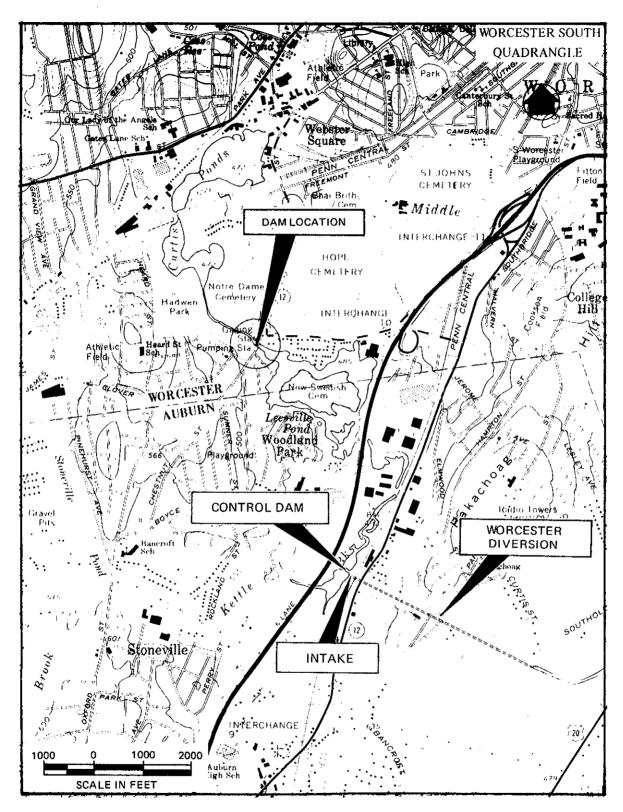
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# OVERVIEW LEESVILLE POND WORCESTER, MASSACHUSETTS



VIEW FROM OXFORD STREET BRIDGE

Location and Direction of Photographs Shown on Figure in Appendix B



LOCATION MAP - LEESVILLE POND DAM

# NATIONAL DAM INSPECTION PROGRAM

#### PHASE I INSPECTION REPORT

#### LEESVILLE POND

#### SECTION 1

#### PROJECT INFORMATION

# 1.1 General

Authority. Public Law 92-367, August 8, 1972, authorized the Secretary of the Army, through the Corps of Engineers, to initiate a national program of dam inspection throughout the United States. The New England Division of the Corps of Engineers has been assigned the responsibility of supervising the inspection of dams within the New England Region. Metcalf & Eddy, Inc. has been retained by the New England Division to inspect and report on selected dams in the State of Massachusetts. Authorization and notice to proceed was issued to Metcalf & Eddy, Inc. under a letter of May 3, 1978, from Ralph T. Garver, Colonel, Corps of Engineers. Contract No. DACW 33-78-C-0306 has been assigned by the Corps of Engineers for this work.

### b. Purposes

- (1) Perform technical inspection and evaluation of non-Federal dams to identify conditions which threaten the public safety and thus permit correction in a timely manner by non-Federal interests.
- (2) Encourage and assist the States to initiate quickly effective dam safety programs for non-Federal dams.
- (3) To update, verify and complete the National Inventory of Dams.

# 1.2 Description of Project

- a. Location. The dam is located in the City of Worcester, Worcester County, Massachusetts, on Kettle Brook, a tributary of the Blackstone River. Approximately 60 percent of Leesville Pond is in the Town of Auburn. (see Location Map, and Watershed Plan, Figure D-1).
- Description of Dam and Appurtenances. Leesville Pond Dam is an earthfill structure approximately 220-feet long and a maximum of 15 feet high (see Appendix B, Figures B-1, B-2, B-3 and B-4). The dam is comprised of a north and south earth embankment section on either side of a concrete and stone masonry spillway. The northern section, which is separated from the spillway by a gated concrete outlet channel, is approximately 60-feet long and 12-feet wide at the crest. The crest consists of a 2-feet wide and 1-foot high concrete cap wall adjacent to a 10-foot wide concrete apron. At the south embankment of the dam section the capwall is 52 feet long, and the concrete apron about 27 feet long. South of the concrete apron the crest of the dam is earth and covered with vegetation. A detailed plan of the dam is shown in Figure B-4, Appendix B.

The maximum elevation of the concrete capwall is 490.5. The concrete apron is at El 489.7. The upstream and downstream slopes of the dam vary from 1:1 to 3:1. The riprap on the south embankment has deteriorated on the upstream slope. A 2-foot-high vertical stone wall is located near the top of the downstream slope. The slopes of the north embankment are entirely overgrown by trees and vegetation.

The spillway is a flat, broad-crested weir constructed of dry-stone masonry and capped with concrete. The crest is 83.6 feet wide and at El 485. The south sidewall of the weir

is concrete, about 20 feet long and 1 foot The north wall, which separates the thick. spillway from the outlet channel, is a concrete-faced stone buttress 25 feet long and about 10-feet wide. Discharge is over the weir, down a cascade, and into a stream bed. As shown in the photograph in Appendix C, the downstream spillway section is comprised of a stepped stone section 55 feet wide, and a smooth-sloped concrete section 29 feet wide. A 4-foot diameter circular opening, possibly an abandoned outlet conduit, was noted through the sloped concrete sec-The opening was probed and found to extend 17.5 feet back into the spillway. intake to this conduit was not visible in the pond. Figure B-3 of Appendix B shows a "waste pipe" at this location.

There is a concrete intake structure located north of the spillway (see Figure B-3 for details). The flared approach channel is 11 feet wide at the gates with 1.3-feet thick concrete training walls that slope into the The bed of the channel is at El 478.4. The intake structure, as shown on the 1936 drawing (Figure B-4), has two 5-foot square wooden slide gates separated by a 1-foot thick wall of concrete and covered by a concrete slab. Two rack and pinion mechanisms are on the upper slab but are not operable. invert of the slide gates in the outlet channel is at El 476.9. The outlet channel is also ll feet wide with concrete sidewalls and is cut in half by a 1-foot-thick sloping concrete wall that extends for 10 feet. The stone and concrete buttress on the south side of the outlet channel has a downstream slope of approximately 2:1. Access to the slide gate mechanism is by a footpath north of the crest of the dam along the shore.

c. Size Classification. Leesville Pond Dam is classified in the "small" category since it has a maximum height of 15 feet and a maximum storage capacity of 415 acre-feet.

- d. Hazard Classification. Leesville Pond is approximately 2,000 feet upstream of Curtis Pond. The area between the two ponds is mostly cemetery property and parkland. In the event of failure of the dam at Leesville Pond, the effect on lives and property immediately downstream of the dam would be small. Accordingly, Leesville Pond Dam has been placed in the "significant" hazard category. However, the resulting flood wave could raise the level of Curtis Pond and could cause failure of the Curtis Pond Dam. Webster Square is immediately downstream from Curtis Pond. This is a highly urbanized area which could experience extensive property damage, and many casualties.
- e. Ownership. The dam was recently acquired by the J. P. Realty Company, 3 Hickory Lane, Auburn, Massachusetts. Mr. Alex Pappas (617-832-3718) granted permission to enter the property and inspect the dam.
- f. Operator. There are no known operators of the dam. The wooden slide gates appear to be inoperable due to rotted timber gate stems and missing parts on the gate mechanism.
- g. Purpose of the Dam. The dam was most recently used as a storage pond for fire protection by the Worcester Rendering Company, a subsidiary of Consolidated Rendering Co., 18 Southbridge Street, Auburn, Massachusetts. Water was pumped to a water tower on the Rendering Company property where it was stored for emergency use. The Rendering Company has since closed, and the pond is now principally used for recreation.
- h. Design and Construction History. A timber dam was originally built on Kettle Brook sometime prior to 1830. The dam and spillway have been entirely rebuilt since then. Beginning in 1928, construction reports by Worcester County inspectors describe the general condition and repairs needed at the dam.

Portions of the present spillway existed prior to 1928. Several modifications have been made to the dam since then. In 1928, the Worcester County Engineer's office ordered repairs, including reducing the height of the flashboards and reconstructing the timber walkway over the spillway. In addition the County recommended that concrete be placed on the south end of the stepped cascade to prevent collapse of the stonework.

The sloping concrete apron for the spillway was added sometime prior to 1931.

In 1936 plans were submitted to the Worcester County Engineer's office by Consolidated Rendering Company for the proposed installation of the waste gates (slide gates) at the north end of the spillway (see Figure B-3, Appendix B). The plan also shows the former timber crest of the weir, the flashboards, and the location of the waste pipe.

In 1937 the County noted seepage through the top of the concrete apron along the waste pipe and recommended the addition of a concrete core wall upstream of the wooden sheeting. The core wall was to extend into the south abutment and tie into the new gate structure on the north. It was recommended that the wooden weir be replaced with concrete and the waste pipe plugged. Also, the stone walls on the abutments should be raised 2 to 3 feet and an automatic tripping device installed on the flashboard pins.

The County records indicate that not all the aforementioned recommendations were implemented. Nevertheless, the dam was not severely damaged during the 1938 floods.

Alterations at the north abutment of the dam by the R. H. White Construction Company were in progress in 1954. The end product was to consist of building up the concrete walls of the sluiceway and adding a new 25-foot long core wall constructed of 3-inch wood sheeting in a concrete footing, backfilled with an impervious clay core, and capped with concrete.

The wall was under construction when the 1955 floods overtopped the dam by about a foot and washed out both abutments. Modifications after the flood, as shown in Figure B-4, consisted of extending the core wall into each abutment to prevent future washouts. Also at this time the present concrete apron was added to the crest and extended upstream at the approach channel. New riprap was placed on the upstream slope of each abutment.

In 1958 the inspection report noted flooding in the abutting property and the flashboards were ordered lowered or removed. By 1969 the condition of the dam was rated as poor, because of leaks through the spillway, and rotting wood on the gates. A 1973 inspection report by the Massachusetts Department of Public Works (see Appendix B) calls for removal of trees and brush from the embankment and restoration of the downstream slope of the south (left) abutment.

i. Normal Operational Procedure. There are no known operating procedures at this dam. The wooden sections of the rack and pinion mechanism have rotted away, leaving the gates inoperable.

The main spillway is ungated and flows are unrestricted. The former "waste pipe" on the spillway is apparently plugged.

# 1.3 Pertinent Data

a. Drainage Area. Leesville Pond has a drainage area of approximately 20,540 acres (32.1 square miles), with a large number of swamps and ponds. (see Figure D-1 in Appendix D for the relative location of the pond in the watershed). Kettle Brook drains from the north and west and includes five major reservoirs for public

water supply. The brook flows through rural, sparsely developed woodland until it reaches the municipal airport and the Worcester City limits, where there is more residential development. Dark Brook drains from Dark Brook Reservoir in the south to Stoneville Pond where it joins Kettle Brook. This area is also moderately developed. A third stream, Ramshorn Brook, flows through gently rolling, very sparsely developed woodland, north to Pondville Pond and downtown Auburn, and finally to Kettle Brook.

Prior to 1959, high water in the watershed would cause flooding in downtown Worcester in the area of Webster Square. In 1959, the U. S. Army Corps of Engineers completed a major diversion structure about one mile upstream of the dam on a southern extension of the pond (see Location Map). The structure, called the Worcester Diversion, consists of an earth control dam with the crest at El 498 and a concrete ogee spillway section with the top at El 492. Major stream flows as high as to 6,000 cfs are diverted by the spillway to a tunnel and a series of canals that flow east and eventually discharge into the Blackstone River, about 3,500 feet south of the Worcester City limits. The intake of the diversion tunnel is at El 487. Two slide gates on the spillway section discharge normal flows. At the time of the inspection one gate was partly opened. During peak storm periods, however, the gates are closed and all the water is diverted to the tunnel. Detailed information on the Worcester Diversion is provided in U.S. Army Corps of Engineers, Design Memorandum No. 1, Hydrologic Analysis, August 1956.

b. Discharge at the Dam Site. Normal discharge at the dam is over the 83.6-foot-wide spillway, down the stepped and sloped sections of the cascade, and into the stream channel which is approximately 100 feet wide. The channel narrows to about 56 feet at the Webster Street

Bridge. The stream bed which is naturally lined with gravel and cobbles, is at El 475 and slopes to El 472 about 150 feet downstream. Water passes under the Webster Street Bridge through an opening which is 40 feet wide and 10 feet high from the streambed to the bottom of the lowest H beam on the bridge (see Figure B-2, Appendix B).

Downstream of the bridge is a USGS gaging station. Past this the stream flows over a small (about 3 feet high) concrete control dam built across the channel. This section of the stream channel is bounded by a stone wall on the north side and a concrete wall on the south. From there the water flows in a stream to Curtis Ponds.

Hydraulic analyses indicate that the spillway can discharge an estimated 1,594 cfs at El 488.3, which is the elevation of the north abutment of the spillway and the lowest point on the crest of the dam. An outflow test flood of 8,600 cfs (one-half the probable maximum flood minus the flow through the Worcester Diversion) will overtop the dam by a maximum of 5.3 feet. Records at the Worcester County Engineer's office state that the dam was overtopped by about 1 foot in 1955.

Controlled discharge was formerly through the slide gates. These are now closed and no longer operable.

- c. Elevation (feet above Mean Sea Level [MSL]). A benchmark at El 485.0 at the spillway crest was estimated from a U.S.G.S. topographic map.
  - (1) Top dam: 488.3 to 490.5
  - (2) Test flood pool: 493.6
  - (3) Design surcharge (original design): Unknown
  - (4) Full flood control pool: Not Applicable (N/A)

- (5) Recreation pool: 485.0
- (6) Spillway crest (ungated): 485.0
- (7) Upstream portal invert diversion tunnel (Worcester Diversion): 487.0 (upstream diversion spillway crest elevation: 492)
- (8) Stream bed at centerline of dam: 475.1
- (9) Maximum tailwater: 475.9

# d. Reservoir

- (1) Length of maximum pool: 6,800 feet
- (2) Length of recreation pool: 6,800 feet
- (3) Length of flood control pool: N/A

# e. Storage (acre-feet)

- (1) Test flood surcharge: 430 at El 493.6
- (2) Top of dam: 415
- (3) Flood control pool: N/A
- (4) Recreation pool: 250 (Approximate)
- (5) Spillway crest: 250

# f. Reservoir Surface (acres)

- \*(1) Top dam: 50
- \*(2) Test flood pool: 50
  - (3) Flood-control pool: N/A
  - (4) Recreation pool: 50
  - (5) Spillway crest: 50

<sup>\*</sup>Based on the assumption that the surface area will not significantly increase with changes in pond elevation from 485 to 488.3.

#### g. Dam

- (1) Type: Earthfill
- (2) Length: 220 feet
- (3) Height: 15 feet
- (4) Top width: 11 feet
- (5) Side slopes: 1:1 to 3:1
- (6) Zoning: Unknown
- (7) Impervious core: 3-inch wood plank cutoff, backfilled with clay on upstream and downstream sides
- (8) Cutoff: Unknown
- (9) Grout curtain: Unknown

## i. Spillway

- (1) Type: Broad crest
- (2) Length of weir: 83.6 feet
- (3) Crest elevation: 485.0 MSL (assumed bench-mark)
- (4) Gates: None
- (5) Upstream Channel: None
- (6) Downstream Channel: Stone cascade to 50foot wide stream bed
- (7) General: Downstream bridge 150 feet from dam; 40 feet wide, 10-foot high passage for water
- j. Regulating Outlets. The only regulating outlets are the two 5- by 5-foot wooden slide gates at the intake structure. The rack and pinion mechanisms for opening the gates have deteriorated beyond use, and the outlet channel, which runs parallel to the spillway cascade, is clogged with debris.

#### SECTION 2

#### ENGINEERING DATA

2.1 General. The only plans, specifications, or computations available from the Owner or State or County offices relative to the design, construction, or repair of this dam are as follows: 1936 Plan of Waste Gate Works across Leesville Pond, and a 1955 Plan of Reconstruction of Dam on Leesville Pond which shows details of the core wall and concrete apron. Copies are included in Appendix B. Supplementary information for the hydraulic-hydrologic evaluation for the dam was provided in U. S. Army Corps of Engineers "Design Memorandum No. 1", dated August 1956, for the Worcester Diversion. Three plans for this tunnel and the control dam were provided by the Corps, but were not included in this report. The only other data available for this evaluation were visual observations during inspection, review of previous inspection reports, and conversations with the Owner and with personnel from the State and County agencies.

We acknowledge the assistance and cooperation of personnel of the Massachusetts Department of Public Works, Messrs. Willis Regan and Raymond Rochford, and of the Massachusetts Department of Environmental Quality Engineering, Division of Waterways, Messrs. John J. Hannon and Joseph Iagallo.

Also, we acknowledge the cooperation and assistance of personnel from the Worcester County Engineer's Office: Messrs. John O'Toole, Joseph Brazauskas, and Mr. Wallace Lindquist - recently retired from county service.

In addition, we thank Mr. Alex Pappas of the J.P. Realty Co., owners of the dam, who allowed us to inspect the dam and provided us with information on the history of the pond.

- 2.2 Construction Records. The only construction records are those listed in Section 2.1 and included in Appendix B. There are no as-built drawings for the dam.
- 2.3 Operation Records. No operation records are available, and there is no daily record kept of pool elevation or rainfall at the dam site. A USGS gaging station is located about 200 feet downstream from the dam, however.

# 2.4 Evaluation

- a. Availability. There is limited engineering data available due to the age of the dam.
- b. Adequacy. The lack of in-depth engineering data did not allow for a definitive review. Therefore the adequacy of this dam could not be assessed from the standpoint of reviewing design and construction data, but is based primarily on visual inspection, past performance history and sound engineering judgment.
- c. Validity. Comparison of available drawings with the field survey conducted during the Phase I inspection indicates that the information is valid.

#### SECTION 3

#### VISUAL INSPECTION

## 3.1 Findings

- a. General. The Phase I Inspection of the dam at Leesville Pond was performed on July 24, 1978. A copy of the inspection check list is included in Appendix A. Periodic inspections of this dam have been made by others since 1925. A partial listing of these inspections is in Appendix B. An inspection was made in 1973 by personnel from the Massachusetts Department of Public Works and a copy of their report is included in Appendix B also.
- b. Dam. Leesville Pond Dam is an earthfill dam with a wood plank core wall and a reinforced concrete capwall and apron. In general, the concrete is in good condition although there is slight spalling of the concrete at the joints in the capwall. The concrete apron and capwall tie into natural ground at the abutments. abutment area is eroded on both the upstream and downstream slopes. On the upstream slope of the south embankment area, there is some random riprap protecting the face, however, slight slumping of the soil is visible. At the northern upstream face, a few riprap stones are visible. The upstream and downstream slopes of both embankments are overgrown with vegetation, including a number of 12- to 18-inch diameter trees on the upstream face of the south embankment.
- c. Appurtenant Structures. The concrete and stonework on the spillway are in fair to good condition. Holes for flashboard pins are still visible on the weir and there is minor spalling and erosion on the training walls. The concrete face south of the stepped section is in good condition. Seepage is evident at the toe of the north spillway abutment (see Figure B-1). A tree is growing at that location and the seepage appears to be following the roots.

The cascade and downstream channel contain minor amounts of debris especially at the toe of the concrete-faced cascade section.

The outlet structure is in poor condition. The intake to the gates is submerged and there is evidence of cracking along the joints on the training walls and erosion along the water line. The slide gates are presently inoperable and it is not known when they were last used. The rack and pinion mechanisms above the gates are rusted, and the wooden parts have rotted away. There is leakage along the top of both wooden gates. In general the concrete outlet channel is in fair condition with only minor spalling, but the floor of the channel is cluttered with wood and trash. One large and several smaller trees and brush have overgrown the outlet channel.

- d. Reservoir Area. The drainage area is comprised of both heavily populated urban and sparsely developed rural and wooded areas. The Worcester Diversion is located 1-1/4 miles upstream from the dam. Leesville Pond has been divided artificially by this flood control diversion, a culvert under Sword Street in Auburn, and the embankment for Highway I-290, which was added within the last 10 years.
- e. Downstream Channel. The discharge from the spillway flows for about 400 feet down a gravel and cobble streambed with concrete and stone sidewalls. Below 400 feet the natural stream channel flows northwest to Curtis Ponds.
- 3.2 Evaluation. The above findings indicate that the dam has several signs of distress which require attention. It is evident that the dam is not adequately maintained and that deterioration will continue unless action is taken. Recommended measures to improve these conditions are included in Section 7.

#### SECTION 4

#### OPERATING PROCEDURES

- 4.1 Procedures. There are no operating procedures at Leesville Pond Dam.
- Maintenance of Dam. Records indicate that no work has been done on the dam in almost 25 years. The dam is inadequately maintained and appears to have rapidly deteriorated in the last 10 years. The 1973 inspection report by the Massachusetts Department of Public Works (see Appendix B) calls for restoration of the eroded downstream slope at the westerly (southwest) side of the dam, and removal of brush and trees from the embankment, but makes no mention of the existing leakage around the outlet, or the faulty gate mechanism.
- 4.3 Maintenance of Operating Facilities. The outlet mechanism is inoperable. The slide gates are closed and cannot be opened with the existing mechanism.
- 4.4 Description of Any Warning Systems in Effect.
  There are no warning systems in effect at this dam.
- 4.5 Evaluation. There are no operational, maintenance, or warning systems in effect at Leesville Pond Dam. Because this dam is in the "significant" hazard category, the situation should be rectified. A program of operation and maintenance for this dam should be implemented as recommended in Section 7.

#### SECTION 5

#### HYDRAULIC/HYDROLOGIC

## 5.1 Evaluation of Features

a. Design Data. The Probable Maximum Flood (PMF) of 31,000 cfs is based on a U. S. Army Corps of Engineers' Hydrologic Analysis: Blackstone River Flood Control, Worcester Diversion, dated August 1956. By using one-half the PMF and adjusting it for the effect of the Worcester Diversion, the inflow test flood for Leesville Pond was calculated to be 9,160 cfs. After adjusting this inflow for surcharge storage, the maximum discharge rate was established as 8,600 cfs with a water surface at El 493.6, which is 5.3 feet above the north abutment of the spillway (lowest point on the crest of the dam).

The spillway can discharge this rate with the pond at El 485.9, which is below the top of the dam. The existing spillway without flashboards can discharge a flow of 1,594 cfs at El 488.3, the elevation of the north abutment of the spillway.

b. Experience Data. Below is a summary of the highest floods recorded on Kettle Brook at Worcester (1932-1978) which was obtained from the above-referenced Corps of Engineers report and from a review of the gaging station records from 1955 to 1978:

<u>Date</u>	Peak discharge (cis)
August 19, 1955	3,970
March 18, 1936	2,520
September 12, 1954	1,530
March 12, 1936	1,340
September 21, 1938	1,300
January 10, 1935	1,020

Past inspection reports state that the dam was overtopped in the 1955 flood by about 1 foot (El 491+).

ville Pond is over the main spillway and through two wooden gates located at the right abutment (see Figure B-1). The gates, however, are closed and are inoperable and therefore all discharge must be over the main spillway.

The visual inspection on July 24, 1978, found the spillway to be in fair condition. There are minor leaks between the spillway and gate structure and the concrete weir at the spillway shows signs of erosion.

An inspection of the Worcester Diversion on July 24, 1978, found that the dam, spillway, and tunnel are in excellent condition. Flow in Kettle Brook was passing through one of the slide gates. The existing water level was about 3 feet below the weir of the overflow intake.

d. Overtopping Potential. Overtopping of the dam by about 3 feet is expected under an outflow test flood of 8,600 cfs. As noted previously, however, the records on overtopping indicate that the dam was overtopped in 1955 by about 1 foot. The peak discharge for the 1955 flood was 3,970 cfs.

Presently, the Worcester Diversion will divert a significant amount of any storm flow. For example, for a maximum discharge of 6,000 cfs through the diversion plus a spillway flow of 1,594 cfs at Leesville Pond, the maximum discharge of Kettle Brook will be 7,594 cfs without overtopping Leesville Pond Dam. Because this discharge is nearly twice the maximum recorded discharge at this site, the potential for overtopping is remote.

In the event of overtopping, complete failure of the dam could occur. The resulting flood wave could cause significant loss of life and appreciable property damage if Curtis Pond Dam failed.

The outflow discharge rate under failure conditions has been calculated as about 16,000 cfs. This results in a flood wave 12 feet high 1,900 feet downstream from the dam.

#### SECTION 6

#### STRUCTURAL STABILITY

# 6.1 Evaluation of Structural Stability

a. Visual Observations. The evaluation of the structural stability of Leesville Pond Dam is mainly based on the visual inspection conducted on July 24, 1978. As discussed in Section 3, Visual Inspection, there were several visible signs of distress.

It is recommended that a more detailed investigation be initiated to evaluate the stability of the dam and seepage at the downstream toe of the spillway sidewall.

b. Design and Construction Data. Discussions with the Owner and County, and State personnel indicate that there are two plans but no specifications or computations relative to the design or construction of this dam. Furthermore, information on the type, shear strength, and permeability of the soil and/or rock materials of the dam embankment apparently does not exist.

The reconstruction of the Leesville Pond Dam embankment, as shown in Figure B-3, shows a proposed impervious core of wood backfilled with blue clay. This is the only data available on the materials comprising the dam embankment.

c. Operating Records. There is no evidence that instrumentation of any type was ever installed in Leesville Pond Dam. The performance of this dam under prior loading can only be inferred from previous records and physical evidence at the site.

- d. Post-Construction Changes. Leesville Pond Dam has undergone at least three major stages of reconstruction as described in Section 1.2.h., Design and Construction History. There are no as-built drawings for the dam or spillway, however.
- e. Seismic Stability. The dam is located in Seismic Zone No. 2 and in accordance with Phase I "Recommended Guidelines" does not warrant seismic analyses.

#### SECTION 7

#### ASSESSMENT, RECOMMENDATIONS, AND REMEDIAL MEASURES

## 7.1 Dam Assessment

Condition Leesville Pond Dam has undergone a. several stages of reconstruction. Due to its age, the dam was neither designed nor constructed according to current approved state-of-the-art procedures. Based upon the visual inspection at the site, the lack of complete engineering data, and the lack of operational and maintenance information, there are areas of concern which must be corrected to assure the continued performance of the dam. Generally, the dam is considered to be in fair condition, although there are several signs of distress: inoperable slide gates, leakage around the slide gates, seepage at the downstream toe of the north abutment of the spillway, steep embankment slopes near the abutments of the dam, erosion of the downstream slopes on the abutments, erosion of the concrete in the training walls of the outlet intake channel, heavy growth of trees and brush on the dam embankment and downstream areas, slumping and erosion of the soil and lack of sufficient riprap on the upstream face of the dam, and wood and trash debris in the outlet channel and in the stream bed.

Hydraulic analyses indicate that the spillway can discharge a flow of 1,594 cfs at El 488.3 which is the elevation of the concrete abutment on the north end of the spillway and the lowest point on the dam crest. An outflow test flood of 8,600 cfs (half of the probable maximum flood minus the diverted flow) will overtop the main dam by about 3 feet. Previous records at this site indicate the dam was overtopped by 1 foot during the 1955 floods. With the present regulating effects of the upstream flood control structure, it is unlikely that overtopping is any longer a serious hazard.

- b. Adequacy of Information. The lack of in-depth engineering data did not allow for a definitive review. Therefore the adequacy of this dam could not be assessed from the standpoint of reviewing design and construction data, but is based primarily on visual inspection, past performance history and sound engineering judgment.
- c. <u>Urgency</u>. The recommendations and remedial measures outlined below should be implemented by the Owner within one year after receipt of this Phase I Inspection Report.
- d. Need for Additional Information. Additional investigations to further assess the adequacy of the dam and appurtenant structures are outlined below in Section 7.2, Recommendations.
- 7.2 Recommendations. In view of the concerns on the continued performance of this dam, it is recommended that the Owner employ a qualified consultant to:
  - a. Evaluate the stability of the dam, and
  - b. Evaluate the seepage at the north abutment of the spillway.

The recommendations on repairs and maintenance procedures are stated below under Section 7.3, Remedial Measures.

## 7.3 Remedial Measures

- a. Alternatives. An alternative to the recommendations in Section 7.2 and the maintenance procedures itemized below would be draining the reservoir and breaching or removing the dam.
- b. Operating and Maintenance Procedures. The dam and appurtenant structures are not adequately maintained. It is recommended that the Owner accomplish the following:
  - (1) repair the gate mechanism and clear the outlet channel of trash and debris
  - (2) repair the concrete on the approach channel

- (3) cut down trees and clear brush from both embankments, the sides of the outlet channel, and the toe of the north spillway abutment
- (4) repair eroded areas of the downstream face of the abutments, and replace the rip-rap on the upstream face of the dam
- (5) fill in the waste pipe outlet with concrete
- (6) clear wood and trash debris from the stream bed below the spillway cascade
- (7) institute a definite plan for surveillance and a warning system during periods of unusually heavy rains and/or runoff; this should be coordinated with the operators of upstream reservoirs
- (8) implement a systematic program of maintenance inspections. As a minimum, the inspection program should consist of a monthly inspection of the dam and appurtenances, supplemented by additional inspections during and after severe storms. All repairs and maintenance should be undertaken in accordance with all applicable State regulations.
- (9) periodic technical inspections of this dam should be continued on a bi-annual frequency.

# APPENDIX A

# PERIODIC INSPECTION CHECKLIST

## PERIODIC INSPECTION

## PARTY ORGANIZATION

PROJECT Lecsville Pond Dam	DATE July 24, 1978
	TIME 1:00 - 5:00 PM
	WEATHER Sunay - 75°
DARMV.	W.S. ELEV. 485* U.S. DN.S.  *assumed benchmark top of spillway apron, upstream edge
PARTY:	
1. Ed Greco 2. Dick Weber	· · · · · · · · · · · · · · · · · · ·
3. Sue Pierce	
4. Frank Sviokla	9
5. David Cole	
PROJECT FEATURE	INSPECTED BY REMARKS
1. <u>dam</u>	Ed Greco Dick Weber
2. Spillway	Lyle Branagan
3	
4.	
5	
6	
7	
8	
9	
10	

ROJECT FEATURE dam	NAME Ed Greco
ISCIPLINE geotechnical	NAME Dick Weber
Vote: ds = doundiron us = upstran	
AREA EVALUATED	CONDITIONS
AM EMBANKMENT	crest is concrete w/ concrete core wall along ds edge, rami section has some wall partway down ds face
Crest Elevation	partius down ds face
Current Pool Elevation	485
Maximum Impoundment to Date	unKnown
Surface Cracks	joints in concrete core wall- slight spalling
Pavement Condition	none
Movement or Settlement of Crest	none visible
Lateral Movement	none visible
Vertical Alignment	1/2+
Horizontal Alignment	straight
Condition at Abutment and at Concrete Structures	concrete crest + core wall fie into . natural ground
Indications of Movement of Structural Items on Slopes	none visible
Trespassing on Slopes	footpaths to north abutment
Sloughing or Erosion of Slopes or Abutments	west side: erosion on (151 DS slopes near abuting the wind around ground tree + brush growth both sides on us+ DS fac
Rock Slope Protection - Riprap Failures	south side: random rip rap us face il stur some overgrown w/ brush north side: some random rip rap us face
Unusual Movement or Cracking at or near Toes	none visible
Unusual Embankment or Downstream Seepage	none visible
Piping or Boils	none visible
Foundation Drainage Features	none visible
Toe Drains	none visible
Instrumentation System	none visible

PROJECT Leesville Pond Dam	DATE July 24, 1978
PROJECT FEATURE Spillway	NAME Lyle Branagan
project feature <u>spillway</u> DISCIPLINE <u>geotechnical</u>	NAME Ed Green
AREA EVALUATED	CONDITION
OUTLET WORKS - SPILLWAY WEIR, APPROACH AND DISCHARGE CHANNELS	
a. Approach Channel	none
General Condition	none
Loose Rock Overhanging Channel	none
Trees Overhanging Channel	none
Floor of Approach Channel	none
b. Weir and Training Walls	concrete training walls, sloped concrete was support holes for flash board pins of 2' south
General Condition of Concrete	minor spalling + erosion or train ; wils,
Rust or Staining	none visible
Spalling	none visible
Any Visible Reinforcing	none visible
Any Seepage or Efflorescence	none visible
Drain Holes	none visible
c. Discharge Channel *	cascade stone spillway
General Condition	fair
Loose Rock Overhanging Channel	none
Trees Overhanging Channel	tree it toe of north sidewall - seepage
Floor of Channel	from stonework at roots stone steps- Journstream is natural stream bed
Other Obstructions	

<sup>\*</sup> southside of spillway is 29ft across, sloped face, with circular 4+t diameter opening, extends 17 ft under spillway crest

PROJECT Leesville Pond Dam	DATE July 24, 1978
PROJECT FEATURE approach to slide gate	s NAME Ed Greeo
DISCIPLINE geotechnical	NAME Dick Weber
AREA EVALUATED	CONDITION
OUTLET WORKS - INTAKE CHANNEL AND INTAKE STRUCTURE	concrete sidewalls
a. Approach Channel	
Slope Conditions	not visible
Bottom Conditions	not visible
Rock Slides or Falls	none
Log Boom	none
Debris	none
Condition of Concrete <del>Lining</del>	cracking along joints + 2+ key way on site ands erosion along water line
Drains or Weep Holes	none visible
b. Intake Structure	
Condition of Concrete	see slide gates, A-5
Stop Logs and Slots	

PROJECT Leesville Pond Dam	DATE July 24, 1978
PROJECT FEATURE Slide gates	NAME Ed Greco
DISCIPLINE geotechnical	NAME Dick Weber
AREA EVALUATED	CONDITION
OUTLET WORKS - OUTLET STRUCTURE * AND OUTLET CHANNEL	2 wooden slide gales \$'x5' concrete sidewalls + overhead slab w/rack + pinon mechanisms
General Condition of Concrete	Aur - minor spalling - cracking
Rust or Staining	nove
Spalling	minor local spalling
Erosion or Cavitation	minor erosion of concrete along water line
Visible Reinforcing	none
Any Seepage or Efflorescence	laskage along top of both still gairs
Condition at Joints	minor spalling
Drain Holes	none visible
Channel	concrete bottom + sidewalls
Loose Rock or Trees Over- hanging Channel	I large + several smaller trees + briss
Condition of Discharge Channel	Scattered wood + trosh debris

## APPENDIX B

	Page
Figure B-1, Plan of Dam	B-1
Figure B-2, Sections	B-2
Figure B-3, Plan of Waste Gate Works Across Leesville Pond, filed December 1936	In Pocket
Figure B-4, Plan of Reconstruction of Dam on Leesville Pond, filed December 1955	In Pocket
Previous Inspections (Partial Listing)	B <b>-</b> 5
Letter Report to Mr. Eli Jacobson	B-7
Inspection Report from Massachusetts Department of Public Works, January 1973	B <b>-</b> 8

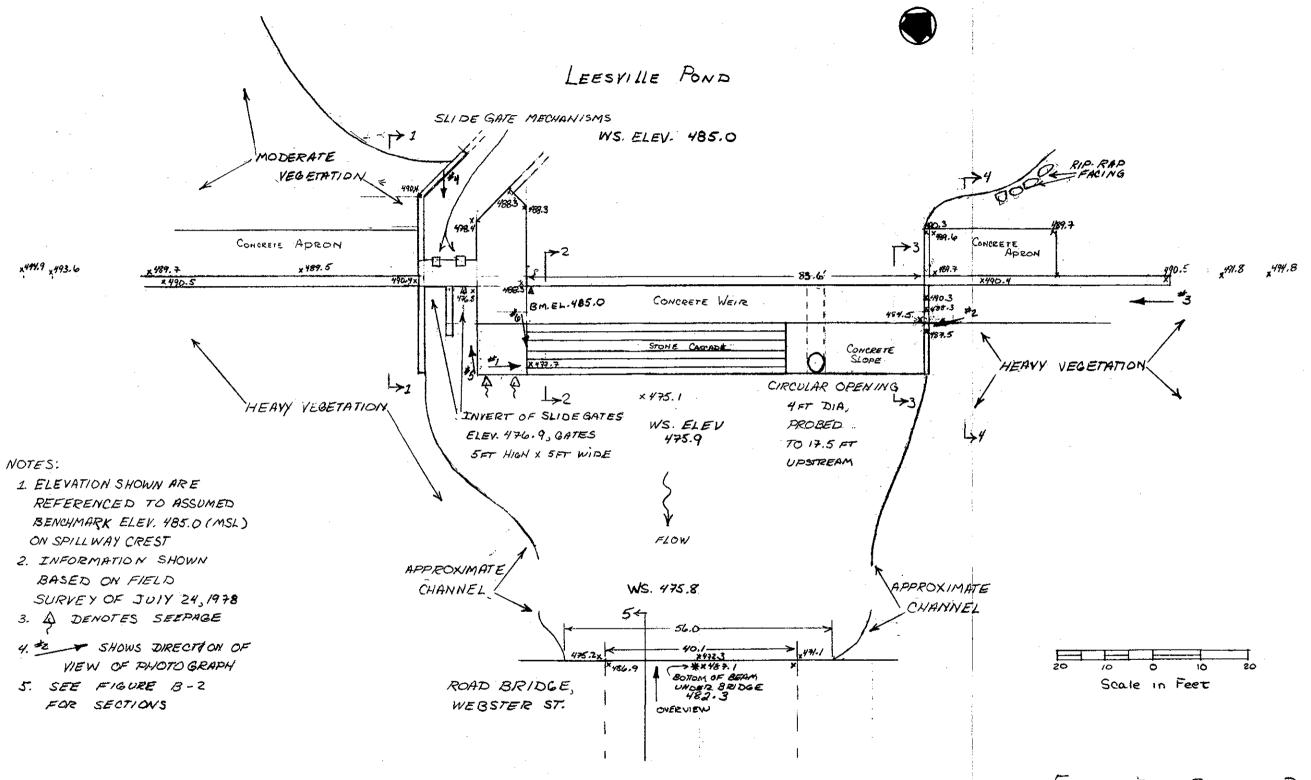
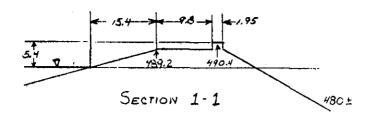
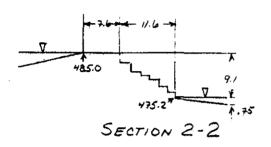
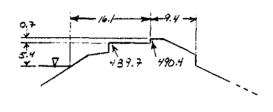


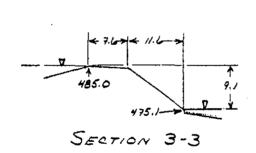
FIGURE B-1 PLAN OF DAM

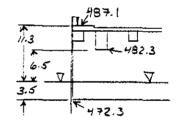




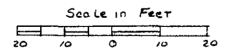


SECTION 4-4



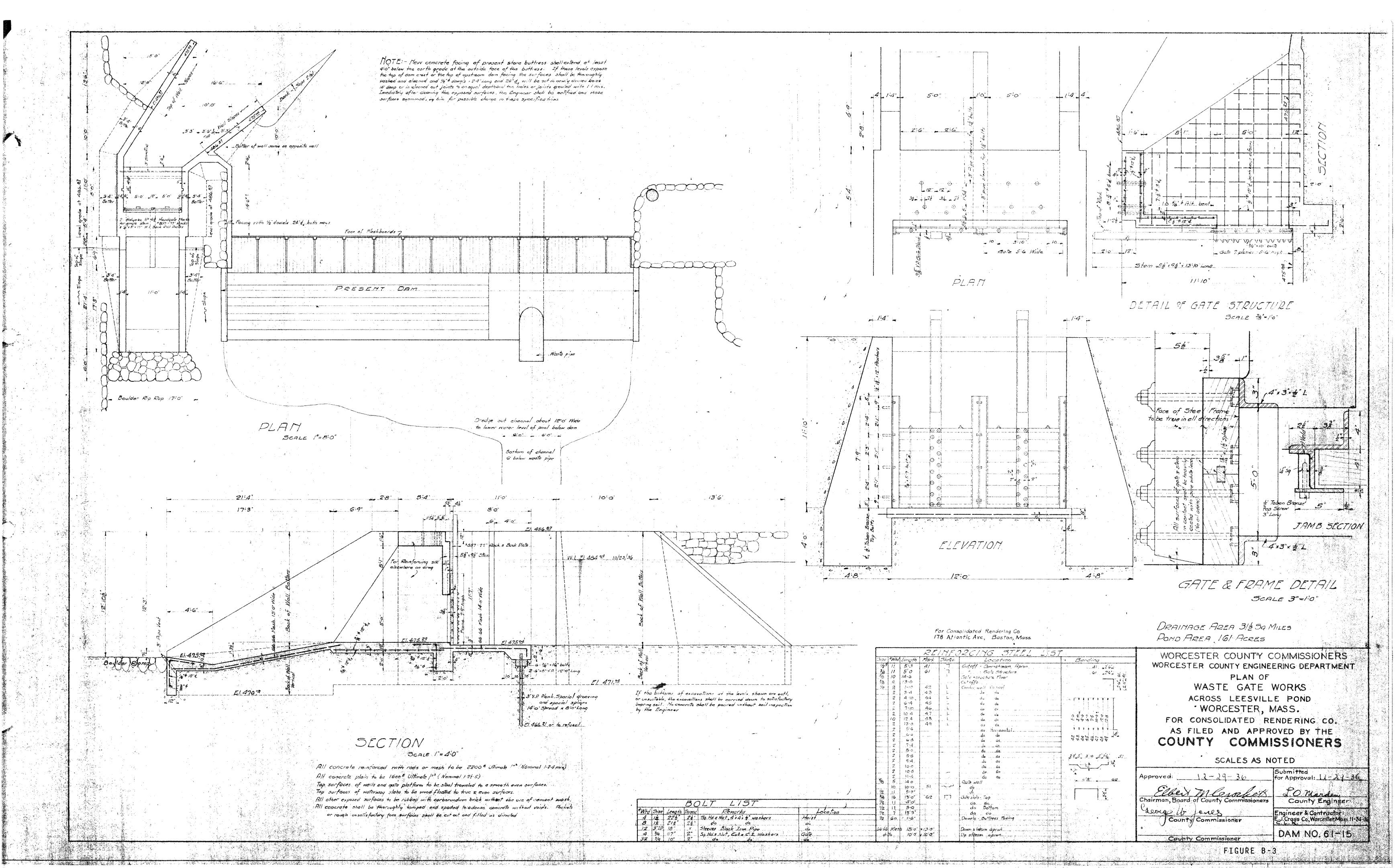


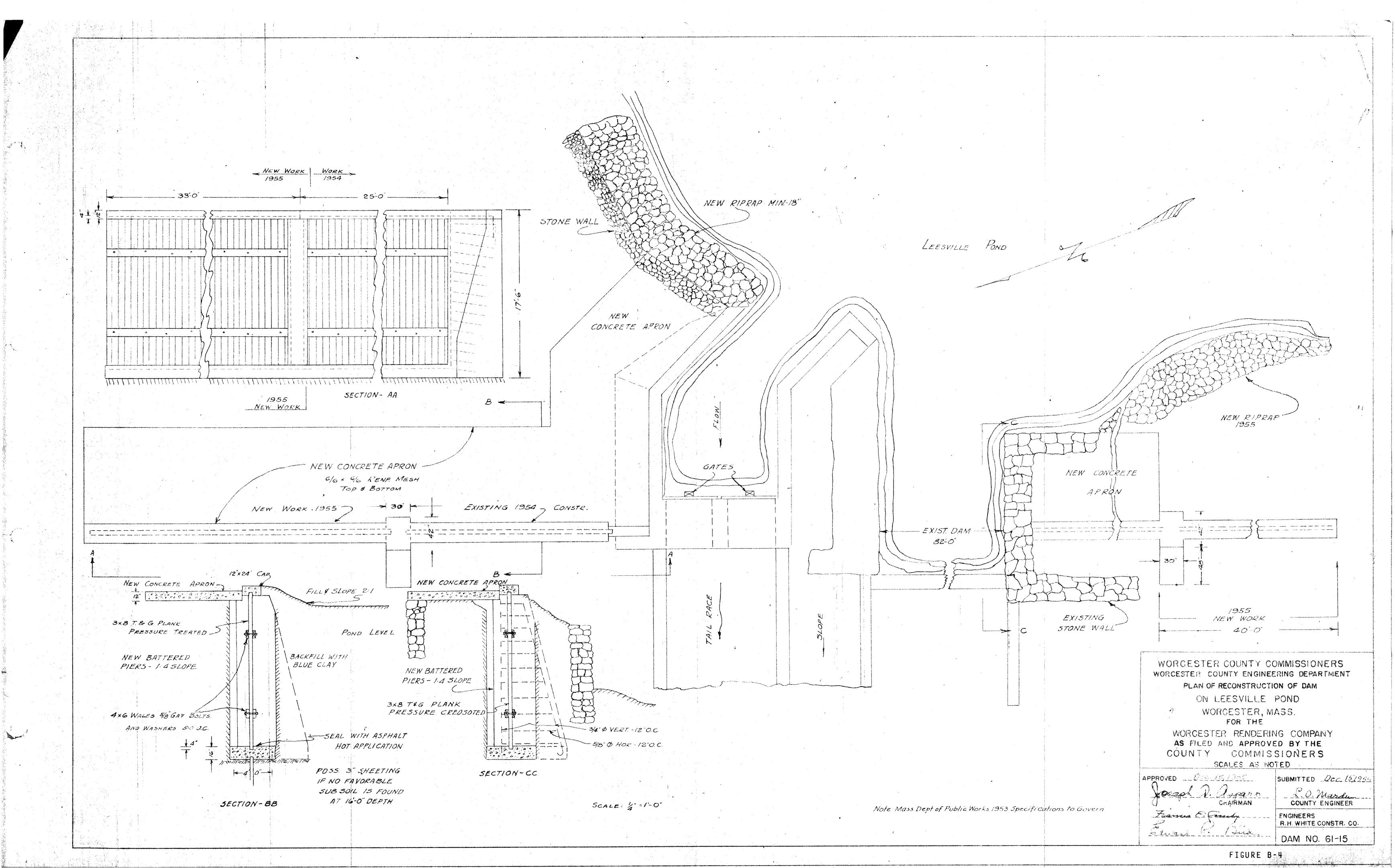
SECTION 5-5



Metaalf & EDDYS INC

FIGURE B-2 SECTIONS





PLAN NO. TOWN OR CITY Woreester DECREE, NO. Leesville pond - Webster St. LOCATION C. C. DOCKET NO. Type Earth Stepped Stone spillway 65 - vert. walls- 29. Name of Main Stream Length " any other Streams /5o'± Height Traced and Approved, Length of Watershed 123 Thickness top Width " 20°± bottom shill - So't is Watershed Cultivated 3.5 \* Downstream Slope Percent in Forests Upstream Steepness of Slope Ledge - Hardpan shed 31.27 Sz. M Length of Spillway Kind of Soil Size of Gates Acres In Watershed أوجو N " " " Reservoir Location of Gates Flashboards used El. 99.0 Length of Reservoir Width Flashboards or Gates Wigth " Dam designed by Max Flow Cu. Ft. per Sec. Un Known. " constructed by Head or Flashboards-Low Water Year constructed Lowell Fertilizer Co-OWNETS. Inspected : Feb. 25, 1929 L. O. Marden. 1928 Worcester Rendering Co., Owners. \*18 South bridge Str. Worcelly OWNER-ELI JACOBSON - 5 ROLLINGWOOD DIC. R. Cross, Mr. Seeman (oucr

#### PREVIOUS INSPECTIONS (PARTIAL LISTING)

COPY OF INSPECTION CARD ON FILE AT THE MASSACHUSETTS DEPARTMENT OF PUBLIC WORKS, DISTRICT OFFICE, WORCESTER.

```
Inspected: Jan. 6, 1937 - L.O. M., E.M. Crockett

New Plans & Specs approved: 12-29-36 by C.C.

Inspected: Nov. 23, 1935 L.O.M., Cross & Mr. Fish

" : April 14, 1936' " , Mr. Fish

" : June 23, 1937' " , E. M. Crockett

" : Nov. 18, 1938' L. H. Spotford

" : Dec. 9, 1940

" : Dec. 11, 1945 - W.O. Lindquist

1936 Repaires: New gates & frame
```

B-6

Apr11 2, 1973

Hr. Eld Jesobson 5 Pollidagres 1 Drivo Moreoster, Massechusetta

RE: Inspection-Dan/3-14-348-15
Horostor
Leasville Ren

Bar Er. Jecobson:

In engineer from the Massachusetts Repartment of Public Works has inspected the above that, of thich you are the exact.

The inspection was made in accordance with Chapter 253 of the Massaciaseetts General Laws, as amended by Chapter 595 of the Actor 1970.

The remains of the increation inchests that this day is case; however, the following conditions were noted that require attentions

- 1. Restore the eroded domestreem alope at the restortly side of the dam.
- 2. Remove the growth of these and brush from the assentment.

to call those conditions to your attention now, tolore they become corieus and emperative to correct.

Yory truly yours,

FIFTH. C. SCHLEH, P.E. Direct Chief Expired

1.604

Lii/ala co: G. H. Lybrand Hill/3 A. Trolano Liab/3

#### INSPECTION REPORT - DAMS AND RESERVOIRS

ı.	Location: City/Town Wasces	TIFIZ Dam No. 3-14-348-15
	Name of Dam LEESVILLE	Inspected by Jananus Michael
		Date of Inspection 1-23-73
2.	Owner/s: per: Assessors	Prev. Inspection
		Pers. Contact
	Name St. & No.	City/Town State Tel. No.
	2.	City/Town State Tel, No.
	Name St. S No.	City/Town State Tel. No.
3.		ntendent, plant manager, appointed
•	by absentee owner, appointed by	
٠	Name:	St. & No.:
	City/Town:	State: Tel.No.:
4.	No. of Pictures taken	
5.	Degree of Hazard: (if dam should	ld fail completely)*
	1. Kinor	2. Noderate
	3. Severe	4. Disastrous
		nd use changes (future development)
6.		Manual
•		
		yes;No.
•	Comments:	
7.	Upstream Face of Dam: Condition	11
	1. Good _	2. Miner Repairs
	3. Major	Repairs 4. Urgent Repairs
0.5	Comments	

Trash and/or debis impeding flow Small Mar of DEBES

Clogged or blocked spillway Vovu

Other

NUNG

Erosion Some on Downstain Shore Bamun Bethiune WALL on LEFT

Cracked or Damaged Masonry Non-

Evidence of Seepage None

Evidence of Piping \_\_\_\_\_

12. Remarks and Recommendations: (Fully Explain)

THE OFWEATH GENERAL CONDITION OF THE

DAM IS GOOD; THERE IS SOME DESIS ON THE DOWNSTROOM M

FACE OF DAM THAT SHOULD BY ROMOVOD. ECOSION OF

THE SLOPE ON THE LEFT SIDE OF THE DOWNSTROAM FACE

OF THE DAM SHOULD BY COLLEGETED. THE CONCLORE

SECTIONS OF THE DAM AND THE DOUBLE CATE CHANGER

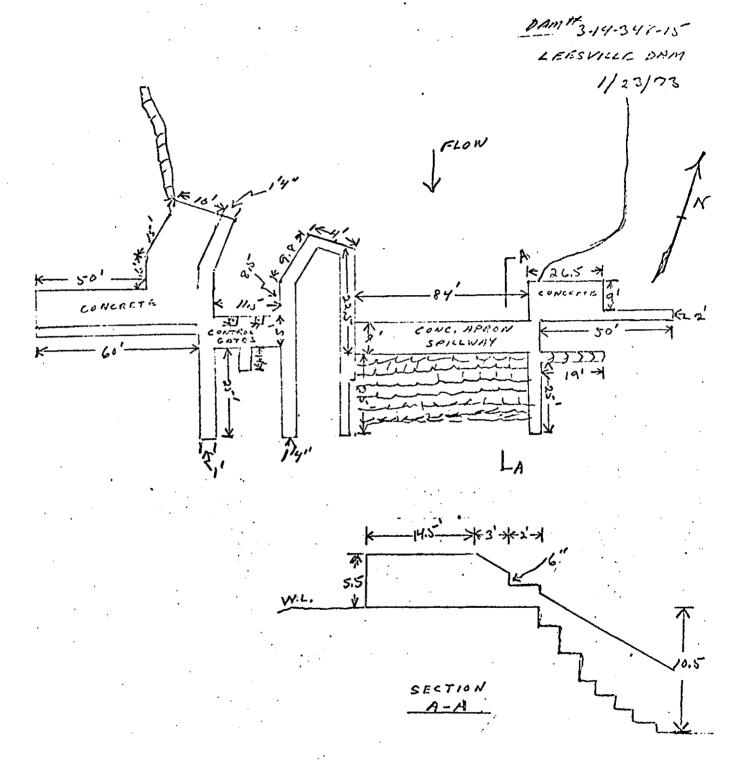
APPEAR TO BE IN GOOD CONSITION.

13.	Overel	17	Cond	1110	1 2

1.	Sef.e
2.	Minor repairs needed
3.	Conditionally safe - major repairs needed
4.	Unsafe
5.	Reservoir impoundment no longer exists (explain)
	Description 1 Community 14th

### DESCRIPTION OF DAM-

			DISTRICT	·
Sul	builted by Donahus, Michaus	Dam No.		
Dat	te	City/Tov	IN WORCESTER	•
		Name of	Dam Lagsylcic	DAM
1.	Location: Topo Sheet No. 2	iB		
	Provide 82" x 11" in clear cop Dam clearly indicated.	y of topo	map with location	of
2.	Year built: Year/s of	subsequen:	t repairs	
3.	Purpose of Dam: Water Supply	l	Recreational	····
	Irrigation	· · · · · · · · · · · · · · · · · · ·	Other	
4.	Drainage Area: 31,27	sq. mi		acres
5.	Normal Ponding Area: 2 C	acres;	kve. depth	
	Impoundment:	_gals.; _		acre ft.
6.	No. and type of dwellings locat	_		rvoir
7.	Dimensions of Dam: Length			16'
	Slopes: Upstream Face	1 ( Voter	•	
	Downstream Face	11.	•	
	. Width across top		•	
8.	Classification of Dam by Materi	ál:		
	Earth Conc. Masonry		Stone Masonry	<b>1</b>
	Timber Rockfill		Other	
9.	A. Description of present land	usage do	unstream of dams	
	% rural;/0	<u> </u>	ırban.	
	B. Is there a storage area or could accomodate the impoundam failure? yes	dment in t	the event of a comp	



					DAM NO. 35/4-378-73
10.	Risk	to life	and propert	ty in event of compl	ete failure.
		No. of	people	20	
		No. of	homes	5	
	•	No. of	Businesses		•
		No. of	industries	1°. x	Type
		No. of	utilities _	· NON-	Type
		Railro	ads	0.00	
			dams		
					•
11.		h Sketch " x 11"		this form showing s	ection and plan
12.	How t	O Locate	e Weast	er St Past Hora	AVE APPROX. 200 :

## APPENDIX C

PHOTOGRAPHS



NO. 1 VIEW OF SPILLWAY CASCADE FROM NORTH ABUTMENT



NO. 2 VIEW OF SPILLWAY FROM SOUTH ABUTMENT



NO. 3 VIEW OF DAM CREST FROM SOUTH ABUTMENT



NO. 4 VIEW OF INTAKE CHANNEL



NO. 5 VIEW OF DISCHARGE CHANNEL AND SLIDE GATES



NO. 6 VIEW OF CHANNEL DOWNSTREAM OF DAM

### APPENDIX D

## HYDROLOGIC AND HYDRAULIC COMPUTATIONS

	<u>rage</u>
Computations	D-1
Figure D-1 Watershed Plan	In pocket

Project NATIONAL REVIEW OF NONFED DAMS Acct. No. 5864

Subject WORCE: TFR MASS AREA Comptd. By LEB Date 7/13/78

Detail LEESVILLE POND DAM CK'd. By RW Date 9/10/79

## (I) Inflow Test Flood \$ 100 Year Flowd

A-Data taken from U.S.C. of E. Report:

Blackstone River Flood Control

Worcester Diversion

Design Memorandum No.1

Hydrologic Analysis American

P.M.P. based flood gives 31,000 cfs as peak which would be based on a 24.32 with varifull in 24 hours with a max. Chair varie of 19 wides & 3he max of 14.25 wiches. The Design Storm used in the project (SPF) had a Peak of 8000 cfs and is based on a 11.0 with 24 name, a max. The variety 8.35 with and a max. The variety 6.68 with Drawing area is 32.1 sq. mile.

B-Due to low height of dam use & PMF as InflowTest 1 cont.

1. Possible Inflow Test Flood = 15500 45. (Most diversion)

C- Diversion Effect

About Coff report provides a ration cares fraduction.

Tunnel & control dam just up stream of telesville Dam. At 15500 cfs

the pond level at the diversion is El. 501. The & of the tunnel exit 15 81 911

Under an BG' head the diversion flow is 6340 cfs. Subfracting the

Evon 15500 cfs gives.

". Inflow Test Flood = 9160 do

## D- 100 Year Flood

For 4.7 miches of rain in Chours, less a minimal infiltration loss of 1.1 miche, the 100 year flood inflow peaks:

Real Inflow Plus = 31000 (4.7-1.1) = 6234 cfs.

Patery curve of chuerson structure and control dan indicates that with this rate of whilever, the deversion would be about 6000 c.f.c.

Thus Inflow 100 year flood = 234 c.f.s.

E - Storage Function

For Inflow Test Flood: Pout = 9160 - 9160 (5) = 9160 - 964 5'-FT

Project Nat. Review of Non Fed Duns	Acct. No. 5864 Page	of <u>-5</u>
Subject Wovcester Mars Area	Comptd. By (FB Date	7/25/70
Detail LEESVILLE POND DAM	. Ck'd. By R W Date	8 10 79

Pond Elev	$\Phi_{s}$	Qc	Prot.	5	FTF
485	0		0	0	
486	262	\$414\ <u>-</u> .	262	. 037	
487	741	وه مستوبیتین	741	.082	
488	1361	Management .	1361	.135	
488.33	1594		1594		
489	2096	18	2114	,194	
490	2929	72	3001	,262	
491	3821	246	4097	,336	
492	4852	758	5610	.419	8756
493 493.6 494	5928 6608 7074	1464 1960 2317	7392 8568 9391	.508 .566 .606	8670 8614 8576

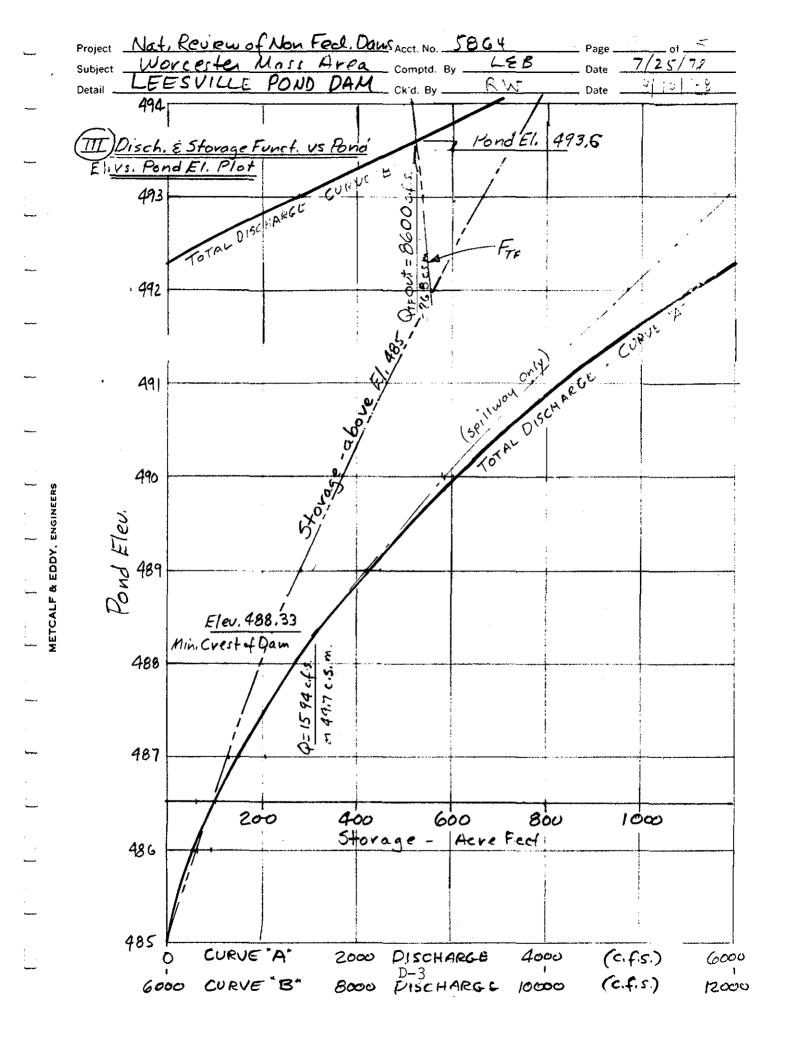
5 = Pond Storage in terms of Inches on total chainage area

D = Depth in pond above spillway crest in feet (D = Hs)

Pondarea = 0.09 in 2@elev. 485 to 0.14 mi2@elev. 490

i. Area = [0.09 + D(.01)] mi2

\$ 5 = 12 \left( \frac{.09 + D.01}{32.1} \right) D



Project Nat. Review of Non Fed. Dams Acct. No. 5864

Subject Worcester, Mass. A) rea Comptd. By LEB Date 7/25/78

Detail LEESVILLE POND DAM Ckid. By Date 3/10/18

## IV Crest Flow

Under Test Flood Discharge:

Total Pour = 8600 (from Item )

Spillway = 6493

Total Crest Flow: 2193

Depth above Crest 2 = 3',  $g_c = 2.55(3)'' = 13.25 cfs/ff$ . Crit. Depth for  $g_c$ ,  $g_c = \frac{(13.25)^4}{9} = 1.76'$ Crit Vel. for  $g_c'$ :  $V_c = \frac{13.25}{1.76} = 7.53 fps$ .

## I Low Outlet Discharge

Outlet consider of 2-5'x sluiceways, inv. el. 476,9

Normal Provide Level -el. 235

[he (. Chow. "Open Cham. Hydri ez 698, Fig 17-29]

H = 8.1; Hd = 1.62, g = 56 of /fl.

Total Disch = (5+5) (56) = 560 c.f.s. = 17.44 c.s.m.

Above Disch. is 6.5% of Test Flood outflow

## VI Storage

Pond aven = 0.09 mi = @ El. 485 & 0.14 mi = @ El. 490 Extrapolated as shown:

Pond El.	Area	Incr. Vola(acft.) >	Volume
485	0.09 mi	60,8	0
480 487	0.10	67,2	60.8
469	0.13	1 5 <b>3.6</b> 86.4	281.6
490	0.14 m;	92.8	368.0
491	0.15	99,2	460.8
492 493	0.16	105.6	560,0 665.6
494	0.18	112.0	7.77.6

```
Project Nat Review of NonFed Dams Acct. No. 5864

Subject Worcester Mass, Area Comptd. By LEB
Detail LEESVILLE POND DAM Ckid. By RW
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Failure of Dam
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Peak Failure Flow: Pond Elevation - 488.3 Toe Elevation - 474.5

> Dam Length Subject to Breaching = 139' Wo = 40% (139) = 56

QP = 1.68 Wo (Yo) "= 1.68 (56) (13.8)" = 4800 cts

Storage Volume Released: Storage Above Spillway: From Graph = Storage Below Spillway & (.09) 10.5 (640) = 5 = Total Storage = 5pillway Flow = 1600 cfs; T.W. = 5.8, A=841; Q=6400

Channel Hydraulics: 510pc = 1900 = ,0016; n = ,06 V= 1.47 R 13 5 14 = 1.0 R 43

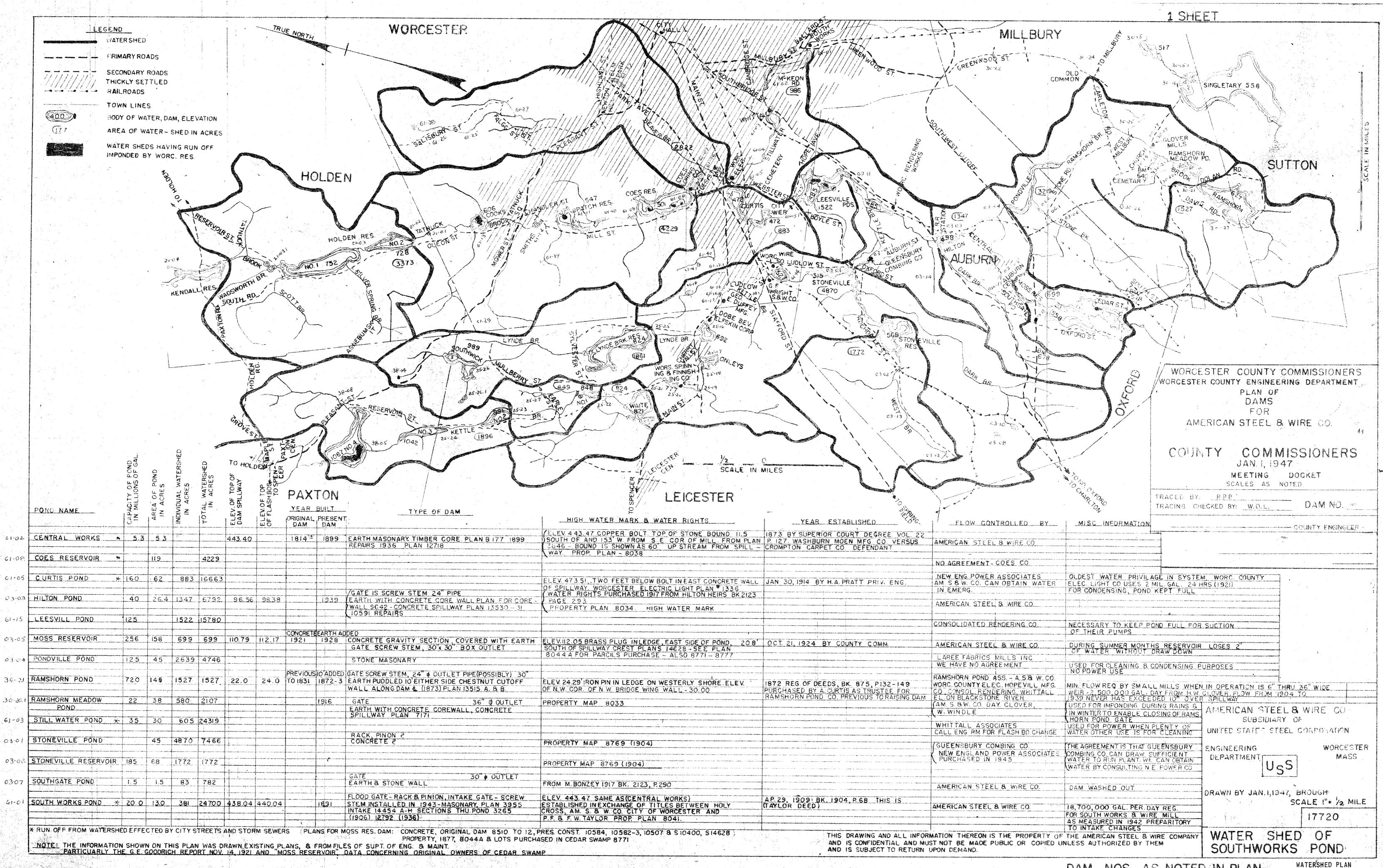
400'	14
4 A P R2/2 V Q	7 13
6 900 300 2.08 2.08 1872	
8 1520 320 2.83 2.83 4295	3/0
10 2180 340 3,45 3.45 7524 12' 2880 360 4,00 4,00 11520	3e'
14' 3620 380 4,50 4,50 16267	
5' 625 250 1.84 1.84 1151	60 5000 10000 15000
Channel Leveth 1900	A. Channel Discharge (c.fs.)

Q = 6400 ; y = 9.4'; A = 1978 AVOI = 50 ac.ft.

Trial Q = 6400 (1 - 50) = 5650 cfc. ; Wave 4+ = 8.9', A= 1812 A= 1895, DV: 46; PFINI = 6400 (1-46)=5700 cts; y=8,9', 4y=3.1'

Time to Drain:

43560 (840)
3600 (1/2) (4800) = 4,2 Hours.



# APPENDIX E INVENTORY FORMS